## Improvements to Southeast Louisiana's floodwalls and pump stations since Katrina: the Hurricane and Storm Damage Risk Reduction System (HSDRRS)

### Pat Fitzpatrick Mississippi State University

- Review of levee failure during Katrina
- Overview of HSDRRS
- Overview of Joint Probability Methods (JPM) used in hazard risk assessment
- JPM application to determining 100-year flood levels for HSDRRS
- HSDRRS concerns

Levee failure timetable Hurricane Katrina











📄 Flooded land









#### New Orleans, August 29, 2005

About two miles west, surge reaches an embankment at the foot of the Orleans Avenue Canal that is 6 feet lower than the floodwalls. Water tops the embankment and pours into City Park.

GENTILLY

10

BUS. (90)

TNA

9 a.m.: Surge rises to 10 feet in the London Avenue Canal and levee wall panels on both sides 1 mile start bending. Water leaks into yards, but the flow is still minor.

LAKEVI

(10)

MID

METAIRIE

OLD METAIRIE

(61)

TIME

(10)

🔵 Flooded land Breach

LEGEND





#### New Orleans, August 29, 2005

**9:45 a.m.:** Several 17th Street Canal levee wall panels fail, releasing a roaring torrent of water into Lakeview. Water from this breach eventually fills much of midtown New Orleans and parts of Metairie.

Breach

MID-CITY

LAKEVIEN

(10)

METAIRIE

OLD METAIRIE

(61)

TIME

(10)

GENTILLY

LEGEND

🔵 Flooded land

(10)

BYWATER

LOWER 9TH WAR

ALGIERS



On the north shore, Katrina makes landfall near Slidell. Storm surge is 15 feet at the Lake Pontchartrain shoreline and reaches more than five miles inland at some points. St. Tammany Parish neighborhoods from the Rigolets all the way to Madisonville are flooded.

ERRYTOWN ENGLISH TURN ENGLISH TURN Poydras DOUBLET POYDRAS 10





# The Hurricane and Storm Damage Risk Reduction System (HSDRRS)

http://www.mvn.usace.army.mil/Missions/HSDRRS.aspx

Four strategic improvements:

- 1) Block five storm surge avenues from 100-year surge
- 2) Raise and strengthen levees and floodwalls
- 3) Make sure designs are consistent
- 4) Improve and stormproof key pump stations

### Some HSDRRS facts

- 350 miles of levees and floodwalls, including interior levees and floodwalls, hundreds of gates and structures for sealing the system
- Armoring against erosion, back-scouring, and at transition points between levees and structures with turf mat topped with sod; research ongoing for other types of armoring
- Clay used for levees is 93 million cubic years (fills 21 Superdomes)
- 78 pumping stations (federal and non-federal)
- Gulf Intracoastal Waterway West Closure Complex;
- Inner Harbor Navigation Canal Surge Barrier; world's largest surge barrier
- Seabrook Floodgate Complex;
- Interim closure structures and pump stations for the three outfall canals



### **Storm Proof Key Pump Stations**







Repair 61 pump stations (\$103 Mil) Storm proof 49 pump stations (\$322 Mil)

Construct 5 safe houses (\$18 Mil)

### Raise and Strengthen Levees / Floodwalls











### Surge barrier ("The Wall")



- 1.8 miles
- 25-26 feet above sea level
- 2 floodgates

## Seabrook floodgate



### Levee expansion, west side of Mississippi River



Joint probability methods for hazard assessment

Synthetic hurricane track dataset

2D wind and pressure fields

Variations for intensity, speed and size

Surge model. Coupling with other relevant water level processes (wave, tide, etc) Determination of elevation—frequency curves at dense points throughout the region using Joint Probability Methods (JPM)

Brute force JPM can require simulations on order of 10,000s Application

Application examples

- Flood Insurance Rate Maps (FIRMs)
- Levee height design
- Elevation or protection design for nuclear plants

### How "100-year" surge event is determined (full JPM)

- Develop probability distributions for each storm parameter (R<sub>max</sub>, intensity, etc.) from observations
- Establish rate of storm occurrence in space and time
- Subdivide each distribution into a small number of discrete pieces (i.e., 6 values)
- Construct all possible hypothetical tracks by taking all possible combinations of the storm quantities. For example, with six values for four parameters one constructs 1296 "storms." (=6 pressure X 6 R<sub>max</sub> X 6 direction X 6 speed)
- Conduct hydrodynamic simulations (surge model, wave coupling, sometimes hydrology) with multiple tracks for each storm type sufficiently spaced for shoreline influence (landfall and bypassing). Track spacing is typically one R<sub>max</sub>, or about ten tracks per site (12,960 simulations)
- For each storm, compute highest surge for locations of interest, tag it with rate of occurrence
- Construct a histogram of rate versus surge height
- Find the 1% surge elevation for each location

## "Optimized sampling" (OS)

- Brute force JPM not feasible using high-resolution hydrodynamic models (i.e., ADCIRC coupled with a wave model)
- JPM-OS techniques seeks to reduce the number of simulations in an intelligent way (fewer combinations, tracks) while maintaining accurate frequency return values

### **Response Surface Method**

- Restricts parameters based on sensitivity response experiments (i.e. only three pressure values chosen). It is found certain combinations are linear, some responses stronger than others, and "smooth"
- Carefully choosing parameters limits combinations, and reduces simulations
- Steps used for JPM-OS-R for HSDRRS design:
  - Step 1: Start with ~5 tracks roughly perpendicular to landfall region and a few values of p and R<sub>max</sub>. Conduct the simulations. Interpolate or extrapolate other surge values in the p-R<sub>max</sub> plane
  - Step 2: Add a few more oblique angles (±45°), simulate on a reduced p-R<sub>max</sub> combination (compared to Step 1), interpolate/extrapolate
  - Step 3: Vary by a few storm speed parameters, simulate on a further reduced p-R<sub>max</sub> combination (compared to Step 2), interpolate/extrapolate
  - Step 4: Interpolate/extrapolate in track space for one p and R<sub>max</sub>
- This process yielded over 50,000 storms.
- Problems with JPM-OS-R are in choosing the proper parameters restrictions (needs expert judgment) which can also be arbitrary; the accuracy of the interpolation; and the use of extrapolation.

### Example of interpolation/extrapolation in Step 1 for one track



Interpolated/extrapolated surge response function in  $\Delta p$ -R<sub>max</sub> plane for one track.  $\Delta p$  is central pressure minus environmental pressure.

Black dots indicate 9 simulated storms for this track. The magenta dashed polygon indicated where bilinear interpolation is performed.

Below 110 mb, and to the right and left of the polygon, the response surface is extrapolated by maintaining a constant  $\Delta p$ -R<sub>max</sub> gradient from the edge of the polygon.

Above 110 mb, the surge response function is extrapolated by maintaining a constant p gradient. JPM-OS-R applied to the post-Katrina New Orleans levees reconstruction Table 1. Summary of the 152 HSDRRS JPM-OS hurricane tracks, stratified by central pressure, radius of maximum winds, translation speed, track direction, primary and secondary plus intensity (Saffir-Simpson scale), and number of stoms in each group. From Jacobsen (2013).

GoM CP mb	GoM R <sub>max</sub> miles	Landfall V <sub>f</sub> mph	θ direction from	Track Set (Number)
	40.9	12.7	Central	P (5)
	28.3	12.7	SE	P (4)
			SW	P (4)
	24.2	12.7	Central	P (5)
	20.9	12.7	SE	P (4)
960			SW	P (4)
	20.4	12.7	Central	S (4)
			SE	S (3)
			SW	S (3)
		6.9	Central	P (5)
				S (4)
	12.7	12.7	Central	P (5)
	29.7	12.7	Central	P (5)
		19.6	Central	P (5)
930	20.4			S (4)
			SE	P (4)
				S (3)
			sw	P (4)
				S (3)
		12.7	Central	P (5)
		6.9	SE	P (4)
				S (3)
			sw	P (4)
				S (3)
	9.2	12.7	Central	P (5)
	25.1	12.7	Central	P (5)
	23.2	12.7	SE	P (4)
	21.2	12.7	SW	P (4)
	20.4	12.7	Central	S (4)
900			SE	S (3)
			SW	S (3)
		6.9	Central	P (5)
				S (4)
	17.1	12.7	Central	P (5)
	14.4	12.7	SE	P (4)
			SW	P (4)
	6.9	12.7	Central	P (5)
				. (9)
3 CP	15 CP-R <sub>max</sub>	19 CP-R <sub>max</sub> -V <sub>f</sub>	30 CPD-R <sub>max</sub> -V <sub>f</sub> -θ	152 Storms



#### Example 100-year surge curves for southshore



#### **Example 100-year surge curves for southshore**

![](_page_35_Figure_1.jpeg)

Test Parameter	Approximate Sensitivity Magnitude (feet)	Notes	
Weirs	2	Dependant on location of weir boundaries	
Wetting and Drying (H0)	0.5	In areas that draw down first	
BFCdLLimit	3	Depends on Manning's n specification, interacts with wind drag	
NOLICA, NOLICAT	0	N/A	
Sector based wind drag formulation	3	Interacts with BFCdLLimit and Manning's n	
Manning's n smoothness	0	N/A	
Land cover data	2	Need accurate data	
Meteorological baseline	2	Need to compare multiple wind models	
Storm Track	2	Closer spacing needed to capture peak in surge response	
Forward Speed	. 3	Becomes increasingly non- linear for locations farther from open Gulf, more uncertainty for slower storms	
Holland B	2	Broad impact	

### HSDRRS concerns

CPRA, 2013: GNO flood protection system notice of construction completion design assessment by Non-Federal Sponsor. DNR Contract File No. 2503-11-61

The Water Institute of the Gulf, 2014: Expert review panel on Greater New Orleans Hurricane and Storm Damage Risk Reduction System Design Guidelines.

### Concerns about the HSDRSS system

- JPM concerns
  - a) Lack of Category 5 hurricane in training set
  - b) Lack of storms tracking from east in training set
  - c) Interpolation/extrapolation used in JPM-OS response function do not guarantee accurate results
  - d) Code had typos (fortunately, very minor impact on results)
  - e) Storm size not explicitly modelled
  - f) Do the sensitivity results add error or have a "cancelling out" effect?
  - g) Future assessments should also include other JPM-OS schemes
- Fortunately, the JPM-OS included a Gaussian residual error term to acknowledge uncertainty and to add some conservativeness. However, it also reduces surge values for lower return periods, which is inconsistent with the philosophy of adding uncertainty.
- Other concerns
  - a) Do "100-year" return levels sufficiently reduce the risk of another flooding event?
  - b) Breaking wave formulations need further evaluation
  - c) Overtopping rate formulation need further evaluation
  - d) Is sea-level rise underestimated? It may be 3-4 feet, and it's not site specific. "Levee lifts" are planned every ten years
  - e) Corps is monitoring of settlement, corrosion, structural integrity, and slope stability. But is more oversight needed?

![](_page_39_Picture_0.jpeg)

Figure 4. Differential settlement at transition between T-Wall for Lake Borgne Closure (background) and earthen Levee for New Orleans east back segment (foreground) - Taken by R. Gilbert on July 16, 2013.

![](_page_40_Picture_0.jpeg)

Figure 5. Shallow slope failure near toe of earthen levee for New Orleans east back segment. Numbered arrows indicate sampling locations for a previous study. (Provided by R. Brouillette, CPRA).

### Future assessment of the HSDRSS system

- The New Orleans risk reduction system is a remarkable engineering achievement, completed relatively quickly in difficult circumstances.
- Also spurred new developments in storm surge modelling and JPM methodologies
- Army Corps of Engineers and all evaluators, however, have noted issues, and have recommended a reanalysis every ten years based on lessons learned, evolving infrastructure issues, and latest science. original analysis 2007/2008, so next one should be completed 2017/2018.