# A Sediment Budget for the Tombigbee River Basin and the Mobile River Basin 

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## Mississippi State University <br> December 2011

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#### Abstract

The purpose of this study is to develop a sediment budget for the Tombigbee River Basin and the Mobile River Basin. A two tier analysis was developed to determine the annual sediment changes along the Tombigbee River Basin (TRB) and the Mobile River Basin (MRB). Results indicate that important sedimentation processes are occurring on the impoundments distributed along the TRB and the Alabama River (ARB) which receives waters from the Cahaba River, Coosa River, and Tallapoosa River. Higher rates of sediment along the lower part of the TRB could be related to the occurrence of river bank instability processes between the Demopolis and the Coffeeville Dams on the Tenn-Tom Waterway. Total sediment loads at the entrance of the Mobile River ranged from 0.8 to 18.75 millions $\mathrm{Mg} \mathrm{yr}^{-1}$. Changes on morphological and hydrodynamic processes below the diversion of the Mobile River in two distributaries can be favoring sedimentation processes along the lower part of the basin and the Mobile Bay. Further analysis is expected to determine the accurate sediment behavior occurring along the lower MRB and its sediment contributions to the Mobile Bay and the Gulf of Mexico.


## Introduction

A sediment budget is an accounting of the sources and disposition of sediment as it travels from its point of origin to its eventual exit from a drainage basin (Stream Systems Technology Center, 2004). Sediment budgets are important in defining the dynamic behavior of a river system (Sharp, 2007). Knowledge of stream and watershed characteristics is important for understanding natural processes and problems associated with watershed management and stream restoration. Sediment production and deposition have been linked to variations in fluvial sediment transport. In many lowland rivers, a major part of sediment is transported in suspension.

The Mobile River is the sixth largest river basin in the United States and the fourth largest in terms of flow (Figure 1). The water resources on the Mobile River Basin (MRB) are influenced by an array of natural and cultural factors, which impart unique and variable qualities to the streams, rivers, and aquifers and provide abundant habitat to sustain the diverse aquatic life in the basin (McPherson et al., 2003). Surface water in the Mobile River Basin generally meets Federal and State drinking water standards and guidelines for protection of aquatic life. However, water quality conditions are adversely affected by urban and agricultural activities, as indicated by elevated concentrations of nutrients, pesticides, and other organic compounds, and biological communities
commonly exhibit signs of environmental stress (Atkins et al., 2004). Approximately $70 \%$ of the MRB is covered by forest and silviculture is the largest industry. Logging and other silviculture activities can significantly contribute high rates of sediment from erosion and runoff.

Assessment of a sediment budget in the MRB is important to increase the scientific understanding of sediment behavior and distribution within the basin as important factors that influence water quality trough the basin itself, the Mobile Bay and the Gulf of Mexico.

## Purpose and Scope

The purpose of this report is to provide an estimate of sediment inflows, outflows and deposition along different sites within the Tombigbee River Basin (TRB) and the Mobile River Basin (MRB).

## Description of the Study Area

The MRB encompasses $113,185 \mathrm{~km}^{2}$ along the states of Mississippi, Alabama, Tennessee and Georgia (Figure 1). The western part of this basin, which is the sixth largest river basin in the United States, is comprised of the TRB $\left(35,674 \mathrm{~km}^{2}\right)$ and the Black Warrior River (BWR - 16,280 $\mathrm{km}^{2}$ ). The eastern MRB is drained by the Alabama River (ARB$58,726 \mathrm{~km}^{2}$ ) which receives waters from the Cahaba River, Coosa River, and Tallapoosa River. The Mobile River is formed by the confluence of the Alabama and Tombigbee Rivers, near Vermont, AL. Downstream from the confluence, the Mobile River flows about 48 km to the south before splitting into several distributaries (Johnson et al., 2002). After flowing across a deltaic plain, these distributaries discharge into the Mobile Bay, which discharges into the Gulf of Mexico (Figure 2).

The mean annual flow in the MRB is about $1760 \mathrm{~m}^{3} \mathrm{~s}^{-1}$. The Alabama and Tombigbee Rivers contribute about 52 and 48\% of the flow, respectively (Atkins et al., 2004). Mean annual runoff and precipitation generally are uniform throughout the MRB, with a highest precipitation amount typically occurring in the northeast part and southern area of the basin. Streamflow in the MRB is highly regulated by upstream impoundments. Around $1,020 \mathrm{~km}^{2}$ of impoundments are extended along the entire basin, some of them constructed for hydroelectric generation and flood control purposes; other series of navigable impoundments were created by completion of the Tennessee Tombigbee Waterway to connect the MRB with the Tennessee River drainage in northeast Mississippi. As a result of this regulation, natural season flow patterns in these tributaries have been altered, with moderated peaks and low flows downstream from the impoundments. Water quality is affected by sediment and nutrients that are trapped in the impoundments and contribute to eutrophication, algal blooms, low oxygen levels and fish killing (Atkins et al., 2004).

Water quality agencies have identified numerous causes and sources of surface water impairment in the MRB. The complex combination of natural (e.g. physiography, geology, soils, climate, hydrology and ecology) and human factors (e.g. built
impoundments, land use changes, mining) within the MRB are considered the principal influences on water quality (Johnson et al., 2002).


Figure 1. Mobile River Basin and principal Subbasins


Figure 2. Topography in the Mobile River Basin.

## Approach

The development of the sediment budget for the TRB and the MRB included the application of a two tiered analysis, based on the proposed sediment budget template developed by Sharp (2007). Initially, data from USGS stations within the MRB in the form of suspended sediment concentrations, suspended sediment loads, instantaneous flow, daily average flow and peak flow were collected. All available data from 1975 to 2010 for all the USGS gauging stations involved in the present study were used. Table 1 presents the USGS stations where data were collected and Figure 1 the location of these stations within the MRB.

All the USGS stations within the Upper Tombigbee River (HUC 03160101), the Middle Tombigbee River (HUC 03160106) and the Middle Tombigbee River-Chickasaw (HUC 03160201) subbasins were evaluated to provide an estimate of sediment inflows, outflows and deposition in the TRB (Figure 3). Results of the sediment budget developed by Sharp (2007) for the Aberdeen Pool were setup as the initial sediment load input for the upper subbasin (HUC 03160101). The sediment load at the outlet of each subbasin was considered as the total sediment load entering the next segment downstream. USGS stations within the same subbasin but not located on the Tombigbee River were used to determine the contribution of flow and sediment loads from tributary watersheds. The entire sediment load of a tributary watershed considered both, accounted and unaccounted areas. The upstream section within a watershed or subbasin contributing at the location of a USGS station was part of the accounted area. The section between the location of a USGS station and the mouth of the watershed, the outlet of a subbasin or a specific location within a subbasin (e.g. entrance of a lake) was considered as the unaccounted area. The sediment load of the accounted area of a watershed or subbasin was divided by its extension providing calculations of mean daily ( $\mathrm{Mg} \mathrm{d}^{-1} \mathrm{~km}^{2}$ ) or mean annual ( $\mathrm{Mg} \mathrm{yr}^{-1} \mathrm{~km}^{2}$ ) sediment yield for Tier 1 and Tier 2, respectively. The unaccounted area of a subbasin or a tributary watershed was considered to have similar sediment yield than the sediment yield observed at the upstream area contributing to a USGS station.

A sediment rating curve (expressed as Equation 1), which represents the relationship between suspended sediment discharges $\left(\mathrm{Q}_{s}\right)$ and the stream or river flow $(\mathrm{Q})$, was developed for the entire dataset within a specific subbasin. The development of the sediment rating curves were the base of both of the tiered analyses, and were used to determine the sediment load generated by each tributary watershed, subbasin or upstream area contributing to a lake.

$$
\mathrm{Q}_{\mathrm{s}}=a \mathrm{Q}^{b} \quad \text { Equation } 1
$$

where
$\mathrm{Q}_{\mathrm{s}}$ is the suspended sediment discharge $\left(\mathrm{Mg} \mathrm{d}^{-1}\right), \mathrm{Q}$ is the observed instantaneous flow ( $\mathrm{m}^{3} \mathrm{~s}^{-1}$ ), and $a$ and $b$ are regression parameters.

The Tier 1 analysis implements basic principles to create an initial sediment budget by determining suspended sediment (SS) loads and yields at the magnitude of the effective discharge, also known as bankfull discharge ( $\mathrm{Q}_{1.5}$ ). A flow frequency distribution was generated from the annual maximum peak flow series at each USGS station by using the
model PKFQWin (Version 5.2). The Q1.5 was calculated from the generated flow frequency distribution (Figure 4, annual exceedance probability=0.6667).


Figure 3. Tombigbee River Basin and subbasins

Table 1. USGS stations used to determine the sediment budget for the Tombigbee River Basin and the Mobile River Basin

| River | Station | Type | Information |
| :---: | :---: | :---: | :---: |
| Tombigbee River | 02437100 \& 02437500 | M | Tombigbee River at Aberdeen, MS |
|  | 02439400 | T | Buttahatchee River nr Aberdeen, MS |
|  | 02441000 | T | Tibbee Creek nr Tibbee, MS |
|  | 02443500 | T | Luxapallila Creek nr Columbus, MS |
|  | 02444160 \& 02444161 | M | Tombigbee River below Bevil L\&D nr Pickensville, AL. |
|  | 02444490 | T | Bogue Chitto Creek near Memphis, AL |
|  | 02444500 | M | Tombigbee River nr Cochrane, AL |
|  | 02446500 | T | Sipsey River nr Elrod, AL |
|  | 02447025 \& 02447026 | M | Tombigbee River below Heflin L\&D nr Gainesville, AL |
|  | 02448000 | T | Noxubee River at Macon, MS |
|  | 02467000 |  | Tombigbee River at Demopolis L\&D nr Coatopa, AL |
|  | $02467500^{1}$ | T | Sucarnoochee River at Livingston, AL |
|  | 02469525 | M | Tombigbee River nr Nanafalia, AL |
|  | 02469761 | M | Tombigbee River below Coffeeville L\&D nr Coffeeville, AL |
| Black Warrior River | 02462501 | M | Black Warrior River below Bankhead L\&D nr Bessemer, AL |
|  | 02465000 | M | Black Warrior River at Northport, AL |
|  | 02466030 \& 02466031 | M | Black Warrior River at Selden L\&D nr Eutaw, AL |
| Coosawattee River | 02380500 | T | Coosawattee River nr Ellijay, GA |
|  | 02383500 | T | Coosawattee River nr Pine Chapel, GA |
|  | 02387500 | M | Oostanaula River at Resaca, GA |
| Alabama River | 02420000 | M | Alabama River nr Montgomery, AL |
|  | 02423000 | M | Alabama River at Selma, AL |
|  | 02428400, 02428401 \& 02429500 | M | Alabama River at Claiborne, AL |
| Mobile River | $02470500^{2}$ | M | Mobile River at Mt Vernon, AL |
|  | 02470629 | D | Mobile River at River Mile 31.0 at Bucks, AL |
|  | 02471019 | D | Tensaw River nr Mt Vernon, AL |



Figure 4. Output file and plot of a flow frequency distribution generated by PKQWin (Ver. 5.2) for USGS stations

The SS load and daily SS yield at the $\mathrm{Q}_{1.5}$ was obtained for each USGS station by using the sediment rating curve developed for each subbasin. Changes on sediment load (erosion or deposition) caused by the presence of an impoundment (e.g. lake) were evaluated by determining a sediment mass balance, which determines amounts of sediment entering the lake, dredging and sediment loadings from the lake.

Tier 2 analysis is a second stage where annual sediment discharges for each station are estimated using its mean daily flow data series. For this study, the used flow data series ranged from 1974 to 2010 when available. The sediment rating equation of each site was used to calculate mean daily SS load values $\left(\mathrm{Mg} \mathrm{d}^{-1}\right)$ from the mean daily flow $\left(\mathrm{m}^{3} \mathrm{~s}^{-1}\right)$. The mean daily SS loads were added for each complete calendar year to provide an annual SS load ( $\mathrm{Mg} \mathrm{yr}^{-1}$ ). A mean annual SS load was generated by averaging annual sediment loads from 1974 to 2010. Once each station has a calculated annual SS load, a SS yield ( $\mathrm{Mg} \mathrm{yr}^{-1} \mathrm{~km}^{2}$ ) was estimated for the contributing area where each station was located. Ungaged areas located downstream of a USGS station were considered to have similar sediment yield that gaged areas, when both areas were located within the same hydrologic unit (watershed) and flow was not routed through a downstream impoundment (dam).

The Tier 2 considers bed load as a percentage of the SS load. The bed load can be estimated as the $20 \%$ of the SS load for locations without the presence of an impoundment, or locations representing the influent of an impoundment. A lower value of $5 \%$ can be considered to calculate effluent flows from any impoundment in this study.

More extended and detailed information about the conceptualization and methodology used to develop a tiered sediment budget analysis is described by Sharp (2007) and Ramirez-Avila (2011).

## Results

Annual sediment loads and yields were calculated based on a two tiered analysis for each USGS station within the TRB, the BWR and the lower Alabama-Coosa-Tallapoosa River Basin (ACT) with enough available sediment and flow dataset (Annex 1). The annual SS load estimations based on the Tier 1 and Tier 2 analyses for four subbasins within the TRB and for the outlets of the BWR and the lower ARB are presented in Tables 2 and 3.

Calculated deposition rates at the Columbus Lake were 10.2 and 3.4 millions $\mathrm{Mg} \mathrm{yr}^{-1}$ of sediment using the Tier 1 and Tier 2, respectively. The Tier 1 deposition rate for the Aliceville Lake was $407,200 \mathrm{Mg} \mathrm{yr}^{-1}$ while the Tier 2 estimation described that the system is balanced when no dredging is performed. For the mass balance estimations reported dredging rates of $100,000 \mathrm{Mg} \mathrm{yr}^{-1}$ and $127,000 \mathrm{Mg} \mathrm{yr}^{-1}$ (McAnally et al., 2004) were considered for the Columbus and Aliceville Lake, respectively.

The sediment load from the BWR, a mixed land use basin, represented only 9\% and 7\% of the sediment load entering to the Mobile River. The relatively low sediment load from this area reflected the influence of impoundments upstream of the subbasin's outlet. Similar observations in the reduction of sediment loads from this subbasin were reported by McPherson et al. (2003).

For both methods of analysis, the Middle Tombigbee River-Chickasaw was the subbasin with the higher annual sediment yield ( $\mathrm{Mg} \mathrm{km}^{-2} \mathrm{yr}^{-1}$ ) within the TRB. Two important structures (Demopolis and Coffeeville Locks and Dams) are located within this subbasin, which could be the key to explain the significant increase in sediment loads occurred between the inlet and the outlet of this area. According to Bankhead et al., (2008) a considerable amount of widening (up to 85 m between 1974 and 2003) has occurred along the length of the Tombigbee River within this subbasin. During their research, areas of high bank erosion were more commonly observed in certain locations with a spatial trend being seen between the dams established in this subbasin. Downstream of Demopolis Dam bank erosion rates were low, but increased up to $3 \mathrm{~m} \mathrm{yr}^{-1}$ along the following 48 km from the dam. Downstream of this length, trends of bank erosion decreased towards Coffeeville Dam, with bank erosion increasing again a few kilometers upstream of the dam. Below Coffeeville Dam, bank erosion rates were high, and then decreased downstream along the following 64 km .

The annual SS load entering the Mobile River after the junction of the Tombigbee/Warrior system with the Alabama River just north of the city of Mobile, AL was estimated as 34 million of Mg and 5.4 million of Mg for the Tier 1 analysis and Tier 2 analysis, respectively. Downstream from the confluence, the Mobile River flows about 48 km to the south before splitting into the Tensaw River and the Mobile River. A USGS station is located on each branch few kilometers after the diversion. The observed reduction in the cumulated magnitude of the SS load for both Tier analyses (Tables 2 and 3 ) was evidenced after estimating the individual load on each station. This reduction (deposition) can be caused by the individual occurrence or the combination of three factors: i) the changes on flow velocity caused by the diversion of the Mobile River; ii) the minimum change of channel slope and the meandering path of the branches from the
diversion to their outlet into the Mobile Bay; and iii) the probable deposition on areas along the deltaic plain during high flow events.

The extension of the entire ACT represented the $53.1 \%$ of the total area contributing to the Mobile River; however, in both analyses the SS load contribution from this basin was 1.8 times smaller than the SS loaded by the Tombigbee/Warrior system. The observed lower sediment loads along the ACT could be attributed to the presence of a significant number of highly regulated impoundments constructed for hydroelectric generation and flood control processes.

For each tiered analysis, a linear relationship between the area of the watersheds and subbasins within the TRB and the BWR and the estimated SS load was determined (Figures 5 and 6). The best fitting observed when using the Tier 1 for estimations can be explained because the SS load variability depends only from the magnitude of the bankfull discharge ( $\mathrm{Q}_{1.5}$ ) after being determined a unique rating curve for each subbasin. For sediment load estimations based on the Tier 2 the change in the mean daily flow on each station along the different years the rating curve was routed (generally from 1974 to 2010) was the factor that affected the reduction in the linear fitting of the dataset.

Although the Tier 2 analysis used the same USGS flow gages that the Tier 1 analysis, the use of daily flow events provides a closer approximation to the natural flow conditions (Sharp, 2007). The occurrence of flows similar to or higher than the bankfull discharge is different for each watershed and subbasin. In the performance of an ongoing study, Avendaño et al. (2012) found that flows with magnitude similar to or above the bankfull discharge represented only the $15 \%$ of the entire flow records for the Buttahatchie River in Mississippi. This condition determines that the application of the Tier 1 generates a significant overprediction of the rate of sediment yield by a specific watershed and/or sediment deposited on specific locations (e.g. Columbus Lake on this study) and further analysis is necessary to perform a more accurate estimation of sediment loads when limited flow data is available.

Considering the application of the Tier 2 as the more accurate method to determine the sediment flux along the different watersheds and subbasins into the MRB, a total sediment load ranging from 0.8 to 18.75 million $\mathrm{Mg} \mathrm{yr}^{-1}$ is expected to enter the Mobile River after the junction of the Alabama and the Tombigbee Rivers (Table 4). Further analysis is needed to determine the rate of reduction of the SS load and the total load of sediment along the distributaries below the Mobile River diversion. When comparing the similar range of dates (2004 to 2010) between the loads at the entrance of the Mobile River and the distributaries the trend to reduce the magnitude of the loads is consistent.

Table 2. Estimation of annual suspended sediment load for different subbasins within the Mobile River Basin based on Tier 1

| Subbasin | Drainage <br> Area* $^{*}$ <br> km$\left.^{2}\right)$ | Area <br> Contribution <br> (\%) | Annual <br> Suspended <br> Sediment <br> Load at Q1.5 <br> (Mg yr $^{-1}$ ) | Suspended <br> Sediment <br> Load <br> Contribution <br> (\%) |
| :---: | :---: | :---: | :---: | :---: |
| Upper Tombigbee River <br> (03160101) | 11,575 | 10.5 | $3,928,845$ | 12 |
| Middle Tombigbee <br> River (03160106) | 23,588 | 21.3 | $7,049,007$ | 21 |
| Lower Black Warrior <br> River (03160113) | 16,280 | 14.7 | $3,014,198$ | 9 |
| Middle Tombigbee <br> River Chickasaw <br> (03160201) | 47,774 | 43.2 | $20,001,609$ | 59 |
| Lower Tombigbee River <br> (03160203) | 51,954 | 46.9 | $21,751,656$ | 64 |
| Lower Alabama River <br> (03150204) | 58,726 | 53.1 | $12,242,934$ | 36 |
| Suspended Sediment <br> Load entering the <br> Mobile River | 110,680 | 100 | $33,994,591$ | 100 |
| Suspended Sediment <br> load at distributaries |  |  | $31,201,756$ |  |

* Including all upstream subbasin's area
${ }^{+}$Ratio of total suspended sediment load entering to the Mobile River in AL.

Table 3. Estimation of annual suspended sediment load for different subbasins within the Mobile River Basin based on Tier 2

| Subbasin | Drainage <br> Area* $^{*}$ <br> $\left.\mathbf{k m}^{\mathbf{2}}\right)$ | Area <br> Contribution <br> $\mathbf{( \% )}$ | Mean Annual <br> Suspended <br> Sediment Load <br> $\left.\mathbf{( M g ~ y r}^{-1}\right)$ | Suspended <br> Sediment <br> Load <br> Contribution <br> $(\%)$ | Mean <br> Annual <br> Bed Load <br> $\left.\mathbf{( M g ~ y r}^{-1}\right)$ | Mean <br> Annual <br> Total Load <br> $\left.\mathbf{( M g ~ y r}^{-1}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Upper Tombigbee River <br> (03160101) | 11,575 | 10.5 | 732,223 | 14 | 146,445 | 878,668 |
| Middle Tombigbee <br> River (03160106) | 23,588 | 21.3 | $3,701,669$ | 69 | 740,334 | $4,442,002$ |
| Lower Black Warrior <br> River (03160113) | 16,280 | 14.7 | 348,827 | 7 | 69,765 | 418,593 |
| Middle Tombigbee <br> River Chickasaw <br> (03160201) | 47,774 | 43.2 | $3,168,627$ | 59 | 633,725 | $3,802,353$ |
| Lower Tombigbee River <br> (03160203) | 51,954 | 46.9 | $3,445,867$ | 64 | 689,173 | $4,135,041$ |
| Lower Alabama River <br> (03150204) | 58,726 | 53.1 | $1,915,331$ | 36 | 383,066 | $2,298,398$ |
| Suspended Sediment <br> Load entering the <br> Mobile River | 110,680 | 100 | $5,361,199$ | 100 | $1,072,240$ | $6,433,438$ |
| Suspended Sediment <br> load at distributaries |  |  | $3,098,150$ |  | $619,630^{\wedge}$ | $1,691,870$ |

* Including all upstream subbasin’s area
${ }^{+}$Ratio of total suspended sediment load entering to the Mobile River in AL
${ }^{\wedge}$ Percentage of sediment load assumed as bed load could be different due to the change on morphological and hydraulic conditions after the diversion

Table 4. Range of sediment loads for the lower subbasins of the Mobile River Basin

| Subbasin | Tombigbee <br> River Output | Alabama <br> River Output | Entering <br> Mobile River | Distributaries ${ }^{*}$ |
| :---: | :---: | :---: | :---: | :---: |
| Maximum SS Load <br> $\left(\mathrm{Mg} \mathrm{yr}^{-1}\right)$ | $11,526,200$ | $4,091,100$ | $15,617,350$ <br> $8,197,719^{*}$ | $5,831,500$ |
| Minimum Load <br> $\left(\mathrm{Mg} \mathrm{yr}^{-1}\right)$ | 548,350 | 251,700 | 800,000 | 587,500 |
| Maximum Bed Load <br> $\left(\mathrm{Mg} \mathrm{yr}^{-1}\right)$ | $2,305,250$ | 818,200 | $3,123,500$ <br> $1,639,544^{*}$ | $1,166,200$ |
| Minimum Bed Load <br> $\left(\mathrm{Mg} \mathrm{yr}^{-1}\right)$ | 109,650 | 50,300 | 16,000 | 117,500 |
| Maximum Total Load <br> $\left(\mathrm{Mg} \mathrm{yr}^{-1}\right)$ | $13,831,450$ | $4,909,300$ | $18,740,850$ <br> $9,837,300^{*}$ | $6,997,700$ |
| Minimum Total Load <br> $\left(\mathrm{Mg} \mathrm{yr}^{-1}\right)$ | 658,000 | 302,000 | 816,000 | 705,000 |
| ${ }^{*}$ Vality |  |  |  |  |

*Values determined only between 2004 and 2010 due to availability of data in one of the USGS stations.


Figure 5. Relation between watershed area and Tier 1 estimated annual suspended sediment load.


Figure 6. Relation between watershed area and Tier 2 estimated annual suspended sediment load.

## Conclusion and Recommendation

From the sediment budget analysis of TRB and the MRB it has been determined that the system is contributing significant amounts of sediment to the impoundments. It was also observed that the system is experiencing an important process of sediment deposition along the lower part of the MRB. Based on sediment contributions from the upstream basin could range between 0.8 and 18.75 millions $\mathrm{Mg} \mathrm{yr}^{-1}$, the sediment deposition along the lower part of the MRB is on the order of 0.1 and 2.85 millions $\mathrm{Mg} \mathrm{yr}^{-1}$. Since the availability of data is limited for the lower part of the Basin and the Bay, where sediment concentration is different due to changes in morphological and hydrodynamic processes, further analysis is needed and the collection of data would be an initial step to facilitate the process. As discussed in the analysis of sediment trends along the upstream basins and the changes on sediments behavior below the Mobile River diversion, the Tier 2 appears to be a reasonable procedure to determine the loads and the trends of sediment processes along the entire watershed. The authors expect to develop a more detailed analysis along the Alabama River Basin to generate more important insights in the behavior of sedimentation processes along the Mobile River Basin.

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#### Abstract

ANNEX


Annex 1.1. Estimation of the Tier 1 suspended sediment load at Q1.5 for USGS stations within the Upper Tombigbee River subbasin (03160101).

|  | Station | Type | Impound | Elevation (amsl) | Drainage Area (km²) | $\begin{gathered} \mathrm{Q}_{1.5} \\ (\mathrm{cms}) \end{gathered}$ | Qs ${ }_{1.5}$ <br> (Mg/d) | SS. Yield ${ }_{1.5}$ <br> (Mg/d/km²) | $\begin{gathered} \text { Total Qs } 1.5 \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | Dredging ( $\mathrm{Mg} / \mathrm{yr}$ ) | Lake Deposition (Mg/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Upper Tombigbee River 03160101 | $\begin{gathered} 02437100 \& \\ 02437500 \text { (Sharp) } \\ \hline \end{gathered}$ | Input |  | 47.2 | 5301.7 | 702.8 | 9292.2 | 1.8 | 10,173,983 |  |  |
|  | MFS | Input |  |  |  | 200.0 | 49.2 |  | 41,520 |  |  |
|  | $\begin{gathered} 02437600 \text { (James } \\ \text { NSL Study) } \\ \hline \end{gathered}$ | Q,Qs |  | 55.5 | 112.0 | 86.8 | 315.6 | 155.0 | 115,188 |  |  |
|  | $02439400$ <br> Buttahatchie River | Q,Qs |  | 67.4 | 2,258.6 | 466.1 | 2178.3 | 1.1 | 868,876 |  |  |
|  | Before Columbus Lake |  |  | 49.4 | 8,600.0 |  |  |  | 12,553,753 |  |  |
|  | 02441000 Tibbee Creek | Q,Qs |  | 47.0 | 2,849.3 | 598.3 | 2,902.7 | 1.2 | 1,258,712 |  |  |
|  | - | Imp | Columbus Lake |  |  |  |  |  |  | 100,000 | 10,153,218 |
|  | 02441390 | Q |  | 30.5 | 11,500.0 | 1,717.1 | 9,751.4 | 0.9 | 3,559,247 |  |  |
|  | MFS | Q |  |  |  | 225.0 | 943.1 |  | 344,249 |  |  |
|  | Upper Tombigbee OUTLET | Outlet |  |  | 11,574.7 |  | 10,764.0 |  | 3,928,845 |  |  |

Annex 1.2. Estimation of Tier 1 suspended sediment load at Q1.5 for USGS stations within the Middle Tombigbee River subbasin (03160106).

|  | Station | Type | Impound | Elevation (amsl) | Drainage <br> Area ( $\mathrm{km}^{2}$ ) | $\begin{gathered} \mathrm{Q}_{1.5} \\ \text { (cms) } \end{gathered}$ | $\begin{gathered} \mathrm{Qs}_{1.5} \\ (\mathrm{Mg} / \mathrm{d}) \end{gathered}$ | SS. Yield 1.5 <br> ( $\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}$ ) | $\begin{gathered} \text { Total Qs } 1.5 \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | Dredging <br> (Mg/yr) | Lake Deposition (Mg/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Middle <br> Tombigbee River 3160106 | Upper Tombigbee Outlet | Input |  |  | 11,574.7 |  | 10,764.0 |  | 3,928,845 |  |  |
|  | $\begin{gathered} 02443500 \\ \text { Luxapallila Creek } \end{gathered}$ | Q, Qs |  | 43.4 | 2,058.6 | 340.7 | 1,781.3 | 0.9 | 715,489 |  |  |
|  | Before Aliceville Lake |  |  |  | 14,800.0 |  |  |  | 5,119,424 |  |  |
|  | - | Imp | Aliceville Lake |  |  |  |  |  |  | 127,000 | 407,212 |
|  | $\begin{gathered} \hline 02444160 \& \\ 02444161 \end{gathered}$ | Q, Qs |  | 30.5 | 1,4892.4 | 1859.0 | 12,562.2 | 0.8 | 4,585,212 |  |  |
|  | 02444490 Bogue Chito Creek | Q, Qs |  | 47.0 | 150.0 | 110.0 | 484.8 | 3.2 | 193,198 |  |  |
|  | 02444500 | Q,Qs |  | 27.4 | 15,384.5 | 1328.9 | 8,536.0 | 0.6 | 3,115,640 |  |  |
|  | $\begin{gathered} \hline 02446500 \\ \text { Sipsey River } \\ \hline \end{gathered}$ | Q, Qs |  | 60.3 | 2,046.5 | 200.7 | 968.9 | 0.7 | 529,248 |  |  |
|  | Before Gainesville Lake |  |  |  | 1,8850.0 |  |  |  | 4,101,360 |  |  |
|  |  | Imp | Gainesville Lake |  |  |  |  |  |  |  | -1,687,011 |
|  | $\begin{gathered} \hline 02447025 \& \\ 02447026 \end{gathered}$ | Q, Qs |  | 19.8 | 18,958.7 | 2276.1 | 15,858.6 | 0.8 | 5,788,371 |  |  |
|  | 02448000 Noxubee River | Q, Qs |  | 43.3 | 3,681.2 | 257.7 | 1,292.1 | 0.4 | 471,632 |  |  |
|  | Middle Tombigbee OUTLET | Outlet |  |  | 23,588.1 |  | 19,359.2 |  | 7,049,007 |  |  |

Annex 1.3. Estimation of the Tier 1 suspended sediment load at Q1.5 for USGS stations within the Middle Tombigbee RiverChickasaw subbasin (03160106).

|  | Station | Type | Impound | $\begin{gathered} \text { Elevation } \\ \text { (amsl) } \end{gathered}$ | Drainage <br> Area (km²) | $\begin{gathered} \mathrm{Q}_{1.5} \\ (\mathrm{cms}) \end{gathered}$ | Qs ${ }_{1.5}$ <br> (Mg/d) | SS. Yield 1.5 ( $\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}$ ) | $\begin{gathered} \text { Total Qs } \mathrm{s}_{1.5} \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | Dredging $(\mathrm{Mg} / \mathrm{yr})$ | Lake Deposition (Mg/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Middle <br> Tombigbee <br> River <br> Chickasaw <br> 03160201 | Middle Tombigbee OUTLET | Input |  |  | 23,588.1 |  | 19,359.2 |  | 7,049,007 |  |  |
|  | 02466030 \& 02466031 BWR | Input |  | 15.2 | 16,280.4 | 1715.4 | 21,430.3 | 1.4 | 3,014,198 |  |  |
|  | 02467000 (Before Demopolis Lake) |  |  |  | 39,868.5 |  |  |  | 10,063,205 |  |  |
|  |  |  | Demopolis Lake |  |  |  |  |  |  |  | -920,821 |
|  | 02467000 | Q, Qs |  |  | 39,909.0 | 2953.4 | 45,020.9 | 1.1 | 16,432,614 |  |  |
|  | 02467500 Sucarnoochee |  |  | 27.4 | 2,405.2 | 161.2 | 846.5 | 0.5 | 472,722 |  |  |
|  | 2469525 (Before Coffeville Lake) |  |  | 0.0 | 45,291.1 |  |  |  | 18,458,074 |  |  |
|  |  |  | Coffeeville |  |  |  |  |  |  |  | -1,512,553 |
|  | 02469761 |  |  | 0.0 | 47,700.0 | 3406.5 | 54,714.0 | 1.1 | 19,970,628 |  |  |
|  | Middle TombigbeeChickasaw OUTLET | Outlet |  |  | 47,774.0 |  | 54,798.9 |  | 20,001,609 |  |  |

Annex 1.4. Estimation of the Tier 1 suspended sediment load at Q1.5 for USGS stations within the Black Warrior River subbasin.

|  | Station | $\begin{array}{\|c\|} \hline \text { Elevation } \\ (\mathrm{amsl})(\mathrm{m}) \end{array}$ | $\begin{array}{\|c\|} \hline \text { Drainage Area } \\ \left(\mathrm{km}^{2}\right) \end{array}$ | Q1.5 (cms) | $\begin{gathered} \hline \mathrm{Qs}_{1.5} \\ (\mathrm{Mg} / \mathrm{d}) \\ \hline \end{gathered}$ | $\begin{array}{\|l\|} \hline \begin{array}{l} \text { SS. Yield } 1.5 \end{array} \\ \left(\mathrm{Mg} / \mathrm{d}^{2} \mathrm{~km}^{2}\right) \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \text { Total Qs } 1.5 \\ (\mathrm{Mg} / \mathrm{yr}) \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Black Warrior River | 02462501 | 52.9 | 10,310 | 1,756 | 2,349 | 0.2 | 857,439 |
|  | 02465000 | 25.4 | 12,484 | 2,648 | 20,810 | 1.7 | 7,595,739 |
|  | 02466030 \& 02466031 | 15.2 | 15,048 | 1,715 | 21,430 | 1.4 | 7,822,062 |
|  | Outlet Lower Black Warrior River | - | 16,280 | 1,715 | 21,430 | 1.4 | 8,642,785 |

Annex 1.5. Estimation of the Tier 1 suspended sediment load at Q1.5 for USGS stations within the Coosawattee River subbasin.

|  | Station | Elevation <br> $(\mathrm{amsl})$ | Drainage <br> Area $\left(\mathrm{km}^{2}\right)$ | $\mathrm{Q}_{1.5}$ <br> $(\mathrm{cms})$ | Qs 1.5 <br> $(\mathrm{Mg} / \mathrm{d})$ | SS. Yield ${ }_{1.5}$ <br> $\left(\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}\right)$ | Total Qs 1.5 <br> $(\mathrm{Mg} / \mathrm{yr})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Coosawattee <br> River | 02380500 | 370.6 | 14,874 | 132 | 2,038 | 0.1 | 744,005 |
|  | 02383500 | 187.8 | 2,127 | 330 | 8,273 | 3.9 | $3,019,746$ |
|  | 02387500 | 184.1 | 4,101 | 490 | 4,358 | 1.1 | $1,590,836$ |

Annex 1.6. Estimation of the Tier 1 suspended sediment load at Q1.5 for USGS stations within the Alabama River subbasin

|  | Station | Elevation <br> $(\mathrm{amsl})$ | Drainage <br> Area $\left(\mathrm{km}^{2}\right)$ | $\mathrm{Q}_{1.5}$ <br> $(\mathrm{cms})$ | Qs 1.5 <br> $(\mathrm{Mg} / \mathrm{d})$ | SS. Yield 1.5 <br> $\left(\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}\right)$ | Total Qs 1.5 <br> $(\mathrm{Mg} / \mathrm{yr})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alabama <br> River | 02420000 | 29.8 | 38,623 | 2,811 | 10,460 | 0.3 | $3,817,902$ |
|  | 02423000 | 18.8 | 43,763 | 2,990 | 18,693 | 0.4 | $6,822,996$ |
|  | 02428400,02428401 <br> $\& 02429500$ | 0.1 | 56,750 | 3,341 | 31,398 | 0.6 | $11,831,024$ |
|  | Outlet Lower <br> Alabama River | 0.1 | 58,726 | 3,341 | 31,398 | 0.6 | $12,242,934$ |

Annex 1.7. Estimation of the Tier 1 suspended sediment load at $\mathrm{Q}_{1.5}$ for the junction of the Tombigbee River and the Alabama River entering to the Mobile River.

|  | Station | Elevation <br> $(\mathrm{amsl})$ | Drainage <br> Area $\left(\mathrm{km}^{2}\right)$ | $\mathrm{Q}_{1.5}$ <br> $(\mathrm{cms})$ | Qs 1.5 <br> $(\mathrm{Mg} / \mathrm{d})$ | SS. Yield ${ }_{1.5}$ <br> $\left(\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}\right)$ | Total Qs <br> $(\mathrm{Mg} / \mathrm{yr})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mobile River | Outlet Lower <br> Tombigbee River | 0.0 | 51,954 | 3,640 | 54,799 | 0.0 | $20,001,609$ |
|  |  <br> 2429500 Alabama | 0.1 | 58,726 | 3,341 | 31,398 | 0.6 | $12,242,934$ |
|  | Entrance to Mobile <br> River | 0.0 | 110,680 | - | 88,341 | 0.8 | $32,244,544$ |

Annex 1.8. Estimation of the Tier 2 annual suspended sediment load, bed load and total load for USGS stations within the Upper Tombigbee River subbasin (03160101).

|  | Input Station | Type | Impound | Lat | Long | $\begin{gathered} \text { Elevation } \\ \text { (amsl) } \end{gathered}$ | Drainage Area $\left(\mathrm{km}^{2}\right)$ | $\begin{gathered} \text { Qs } \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | $\begin{gathered} \text { SS. Yield } \\ \left(\mathrm{Mg} / \mathrm{yr} / \mathrm{km}^{2}\right) \end{gathered}$ | Total Qs (Mg/yr) | $\begin{gathered} \text { Bed } \\ \text { Load } \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | Total Load (Mg/yr) | Dredging <br> (Mg/yr) | Lake Deposition (Mg/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Upper Tombigbee River 03160101 | $\begin{gathered} 02437100 \text { \& } \\ 02437500 \text { (Sharp) } \end{gathered}$ | Input |  | 33.82056 | 88.54639 | 47.2 | 5301.7 | 2,791,341 | 526 | 2,791,341 | 558,268 | 3,349,609 |  |  |
|  | MFS | Input |  |  |  |  |  | 14,771 |  | 14,771 | 2,954 | 17,725 |  |  |
|  | 02437600 <br> (James NSL Study) | Q,Qs |  | 33.81333 | 88.56639 | 55.5 | 112.0 |  | 1,808 | 202,536 | 40,507 | 243,043 |  |  |
|  | 02439400 Buttahatchie River | Q,Qs |  | 33.79000 | 88.26528 | 67.4 | 2258.6 | 54,414 | 26 | 59,464 | 11,893 | 71,356 |  |  |
|  | Before Columbus <br> Lake |  |  | 33.57600 | 88.49200 | 49.4 | 8600.0 |  |  | 3,439,089 | 687,818 | 4,126,907 |  |  |
|  | $\begin{gathered} 02441000 \\ \text { Tibbee Creek } \end{gathered}$ | Q,Qs |  | 33.53778 | 88.63333 | 47.0 | 2849.3 | 89,242 | 37 | 106,024 | 21,205 | 127,229 |  |  |
|  | - | Imp | Columbus Lake |  |  |  |  |  |  |  |  |  | 100,000 | 3,390,262 |
|  | 2441390 | Q |  | 33.51694 | 88.48944 | 30.5 | 11500.0 | 383,249 | 63 | 383,249 | 19,162 | 402,412 |  |  |
|  | MFS | Q |  |  |  |  |  | 344,249 |  | 344,249 | 17,212 | 361,462 |  |  |
|  | Upper Tombigbee OUTLET | Outlet |  |  |  |  | 11574.7 |  |  | 732,223 | 146,445 | 878,668 |  |  |

Annex 1.9. Estimation of the Tier 2 annual suspended sediment load, bed load and total load for USGS stations within within the Middle Tombigbee River subbasin (03160106).

|  | Input Station | Type | Impound | Lat | Long | Elev. (amsl) | Drainage <br> Area <br> $\left(\mathrm{km}^{2}\right)$ | $\begin{gathered} \text { Qs } \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | $\begin{gathered} \text { SS. Yield } \\ \left(\mathrm{Mg} / \mathrm{yr} / \mathrm{km}^{2}\right) \end{gathered}$ | Total Qs (Mg/yr) | $\begin{array}{\|c\|} \hline \text { Bed } \\ \text { Load } \\ (\mathrm{Mg} / \mathrm{yr}) \\ \hline \end{array}$ | Total Load (Mg/yr) | $\begin{gathered} \hline \text { Dredgin } \\ \mathrm{g} \\ (\mathrm{Mg} / \mathrm{yr}) \\ \hline \end{gathered}$ | Lake Deposition (Mg/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Middle } \\ \text { Tombigbee } \\ \text { River } \\ 03160106 \end{gathered}$ | Upper Tombigbee Outlet | Input |  |  |  |  | 11574.7 | 10,764 |  | 732,223 | 146,445 | 878,668 |  |  |
|  | $\begin{gathered} 02443500 \\ \text { Luxapallila Creek } \end{gathered}$ | Q, Qs |  | 33.51417 | 88.39528 | 43.4 | 2058.6 | 32,470 | 18 | 36,096 | 7,219 | 43,315 |  |  |
|  | Before Aliceville Lake |  |  |  |  |  | 14800.0 |  |  | 846,914 | 169,383 | 1,016,297 |  |  |
|  | - | Imp | Aliceville Lake |  |  |  |  |  |  |  |  |  | 127,000 | -108,421 |
|  | 02444160 \& 02444161 | Q, Qs |  | 33.21056 | 88.28861 | 30.5 | 14892.4 | 950,207 | 64 | 950,207 | 47,510 | 997,718 |  |  |
|  | 02444490 Bogue Chito Creek | Q, Qs |  | 33.53778 | 88.63333 | 47.0 | 150.0 | 22,668 | 151 | 24,748 | 4,950 | 29,698 |  |  |
|  | 2444500 | Q,Qs |  | 33.08111 | 88.23722 | 27.4 | 15384.5 | 1,308,452 | 85 | 1,308,452 | 261,690 | 1,570,142 |  |  |
|  | 02446500 Sipsey River | Q, Qs |  | 33.25694 | 88.77639 | 60.3 | 2046.5 | 29,994 | 22 | 44,886 | 8,977 | 53,863 |  |  |
|  | Before Gainesville Lake |  |  |  |  |  | 18850.0 |  |  | 1,522,825 | 304,565 | 1,827,390 |  |  |
|  |  | Imp | Gainesville Lake |  |  |  |  |  |  |  |  |  |  | -1,443,127 |
|  | 02447025 \& 02447026 | Q, Qs |  | 33.85222 | 88.15417 | 19.8 | 18958.7 | 3,114,778 | 164 | 3,114,778 | 155,739 | 3,270,517 |  |  |
|  | $02448000$ <br> Noxubee River | Q, Qs |  | 32.10194 | 88.56167 | 43.3 | 3681.2 | 118,218 | 32 | 172,558 | 34,512 | 207,070 |  |  |
|  | Middle Tombigbee OUTLET | Outlet |  |  |  |  | 23588.1 | 3,666,768 |  | 3,701,669 | 740,334 | 4,442,002 |  |  |

Annex 1.10. Estimation of the Tier 2 annual suspended sediment load, bed load and total load for USGS stations within the Middle Tombigbee River-Chickasaw subbasin (03160201).

|  | Input Station | Type | Impound | Lat | Long | Elev. (amsl) | $\begin{array}{\|c} \hline \text { Drainage } \\ \text { Area } \\ \left(\mathrm{km}^{2}\right) \end{array}$ | $\begin{gathered} \text { Qs } \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | $\left\|\begin{array}{c} \text { SS. Yield } \\ \left(\mathrm{Mg} / \mathrm{yr}^{2} \mathrm{~km}^{2}\right) \end{array}\right\|$ | $\begin{gathered} \hline \text { Total } \\ \text { Qs } \\ (\mathrm{Mg} / \mathrm{yr}) \end{gathered}$ | $\begin{array}{\|c\|} \hline \begin{array}{c} \mathrm{Bed} \\ \mathrm{Load} \\ (\mathrm{Mg} / \mathrm{yr}) \end{array} \\ \hline \end{array}$ | $\begin{gathered} \hline \text { Total } \\ \text { Load } \\ (\mathrm{Mg} / \mathrm{yr}) \\ \hline \end{gathered}$ | Dredging <br> (Mg/yr) | Lake <br> Deposition <br> (Mg/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Middle <br> Tombigbee <br> River <br> Chickasaw <br> 03160201 | Middle Tombigbee OUTLET | Input |  |  |  |  | 23588.1 | 3,666,768 |  | 3,701,669 | 740,334 | 4,442,002 |  |  |
|  | 02466030 \& 02466031 BWR | Input |  | 32.77778 | 87.84056 | 15.2 | 16280.4 | 322,418 | 21 | 348,827 | 69,765 | 418,593 |  |  |
|  | Before Demopolis Lake |  |  |  |  |  | 39868.5 |  |  | 4,050,496 | 810,099 | 4,860,595 |  |  |
|  |  |  | Demopolis Lake |  |  |  |  |  |  |  |  |  |  | 929,839 |
|  | 2467000 |  |  |  |  |  | 39909.0 | 3,275,630 |  | 3,275,630 | 655,126 | 3,930,756 |  |  |
|  | 02467500 Sucarnoochee Creek |  |  | 32.57361 | 88.19333 | 27.4 | 2405.2 | 39,543 | 25 | 60,498 | 12,100 | 72,597 |  |  |
|  | 2469525 (Before Coffeville Lake) |  |  | 32.13000 | 88.04111 | 0.0 | 45291.1 |  |  | 3,642,548 | 728,510 | 4,371,057 |  |  |
|  |  |  | Coffeeville |  |  |  |  |  |  |  |  |  |  | 1,049,152 |
|  | 02469761 \& 02469761 |  |  | 31.75694 | 88.12500 | 0.0 | 47700.0 | 3,163,719 | 66 | 3,163,719 | 158,186 | 3,321,905 |  |  |
|  | Middle Tombigbee-Chickasaw OUTLET | Outlet |  |  |  |  | 47774.0 | 3,168,627 |  | 3,168,627 | 633,725 | 3,802,353 |  |  |

Annex 1.11. Estimation of the Tier 2 annual suspended sediment load, bed load and total load for USGS stations within the Black Warrior River subbasin.

|  | Station | Elevation <br> $(\mathrm{amsl})$ | Drainage <br> Area $\left(\mathrm{km}^{2}\right)$ | $\mathrm{Q}_{1.5}(\mathrm{cms})$ | SS. Yield 1.5 <br> $\left(\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}\right)$ | Total <br> $\mathrm{Qs}(\mathrm{Mg} / \mathrm{yr})$ | Bed <br> Load <br> $(\mathrm{Mg} / \mathrm{yr})$ | Total Load <br> $(\mathrm{Mg} / \mathrm{yr})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Black <br> Warrior <br> River | 2462501 | 52.9 | 10,310 | 52,120 | 5 | 52,120 | 10,424 | 62,545 |
|  | 2465000 | $2466030 \&$ |  |  |  |  |  |  |
| 2466031 |  |  |  |  |  |  |  |  |

Annex 1.12. Estimation of the Tier 2 annual suspended sediment load, bed load and total load for USGS stations within the Coosawattee subbasin

|  | Station | Elevation <br> $(\mathrm{amsl})$ | Drainage <br> Area $\left(\mathrm{km}^{2}\right)$ | Q1.5 $^{(\mathrm{cms})}$ | SS. Yield 1.5 <br> $\left(\mathrm{Mg} / \mathrm{d}^{2} / \mathrm{km}^{2}\right)$ | Total <br> Qs $(\mathrm{Mg} / \mathrm{yr})$ | Bed <br> Load <br> $(\mathrm{Mg} / \mathrm{yr})$ | Total Load <br> $(\mathrm{Mg} / \mathrm{yr})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Coosawattee <br> River | 2380500 | 370.6 | 14,874 | 16,335 | 1 | 16,335 | 3,267 | 19,602 |
|  | 2383500 | 187.8 | 2,127 | 14,723 | 7 | 14,723 | 2,945 | 17,668 |
|  | 2387500 | 184.1 | 4,101 | 28,543 | 7 | 28,543 | 5,709 | 34,252 |

Annex 1.13. Estimation of the Tier 2 annual suspended sediment load, bed load and total load for USGS stations within the Alabama River subbasin

|  | Station | Elevation <br> $(\mathrm{amsl})$ | Drainage <br> Area $\left(\mathrm{km}^{2}\right)$ | $\mathrm{Q}_{1.5}(\mathrm{cms})$ | SS. Yield 1.5 <br> $\left(\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}\right)$ | Total <br> $\mathrm{Qs}(\mathrm{Mg} / \mathrm{yr})$ | Bed <br> Load <br> $(\mathrm{Mg} / \mathrm{yr})$ | Total Load <br> $(\mathrm{Mg} / \mathrm{yr})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alabama <br> River | 2420000 | 29.8 | 38,623 | 607,969 | 16 | 607,969 | 121,594 | 729,562 |
|  | 2423000 | 18.8 | 43,763 | 208,875 | 5 | 208,875 | 41,775 | 250,651 |
|  | 2 |  |  |  |  |  |  |  |
|  | 242400,2428401 | 0.1 | 56,750 | $1,792,862$ | 33 | $1,850,891$ | 370,178 | $2,221,069$ |

Annex 1.14. Estimation of the Tier 1 suspended sediment load at $\mathrm{Q}_{1.5}$ for the junction of the Tombigbee River and the Alabama River entering to the Mobile River

|  | Station | Elevation (amsl) | Drainage <br> Area (km²) | Q1.5 (cms) | SS. Yield ${ }_{1.5}$ ( $\mathrm{Mg} / \mathrm{d} / \mathrm{km}^{2}$ ) | $\begin{gathered} \text { Total } \\ \text { Qs (Mg/yr) } \end{gathered}$ | $\begin{gathered} \hline \text { Bed } \\ \text { Load } \\ (\mathrm{Mg} / \mathrm{yr}) \\ \hline \end{gathered}$ | Total Load (Mg/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mobile River |  |  | 51,954 | 3,168,627 | 66 | 3,168,627 | 633,725 | 3,802,353 |
|  | $\begin{gathered} \hline \text { 2428400, } 2428401 \\ \text { \& 2429500 } \\ \text { Alabama } \end{gathered}$ | 0.1 | 58,726 | 1,792,862 | 33 | 1,915,331 | 383,066 | 2,298,398 |
|  | 02470500 Mobile River | 0.0 | 110,680 | 13,929 | 0.1 | 5,083,959 | 1,016,792 | 6,100,750 |

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MISSISSIPPI STATE


